

DEFORMABLE MIRRORS FOR WAVEFRONT TOMOGRAPHY

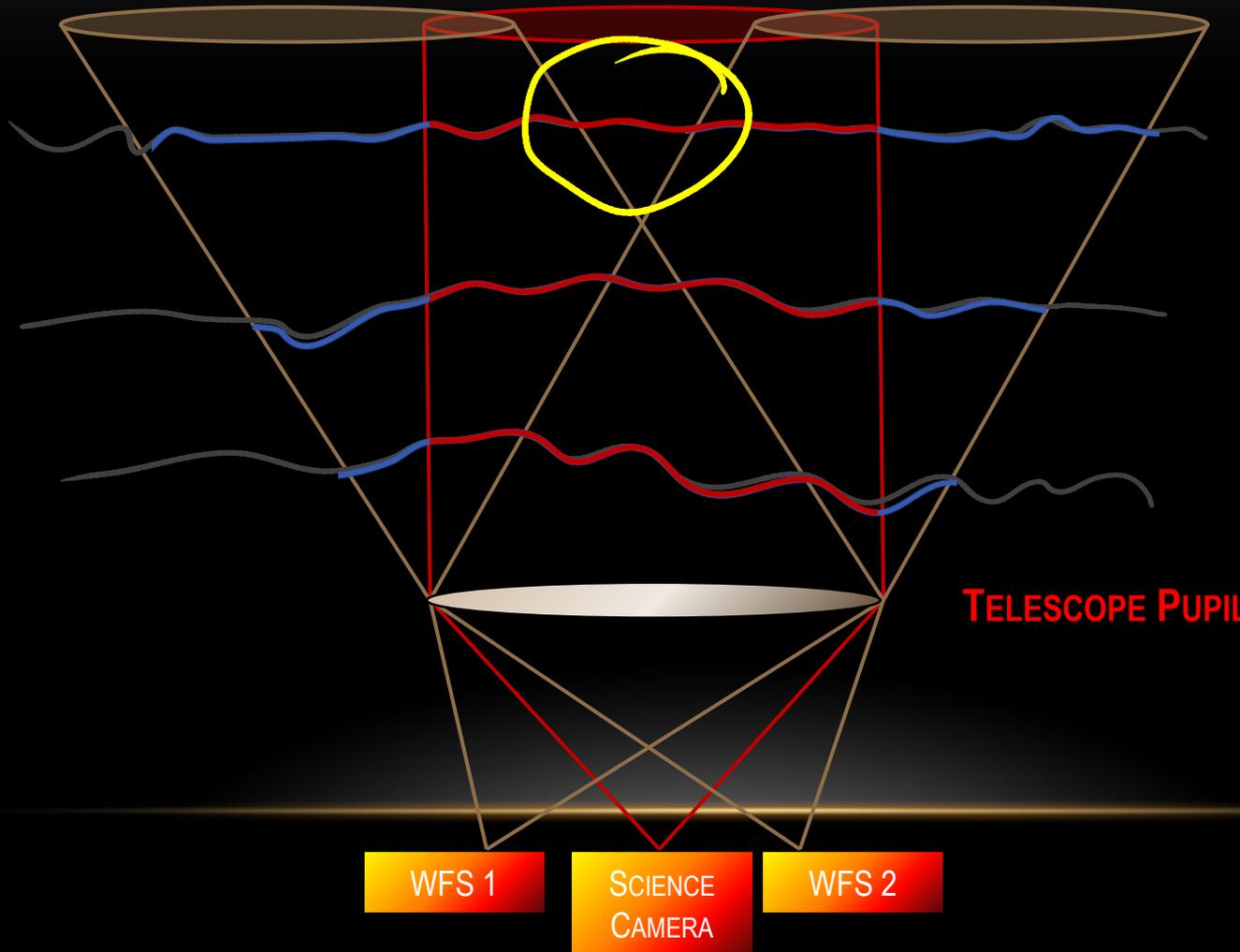
Tim Morris

University of Durham, UK

INTRODUCTION

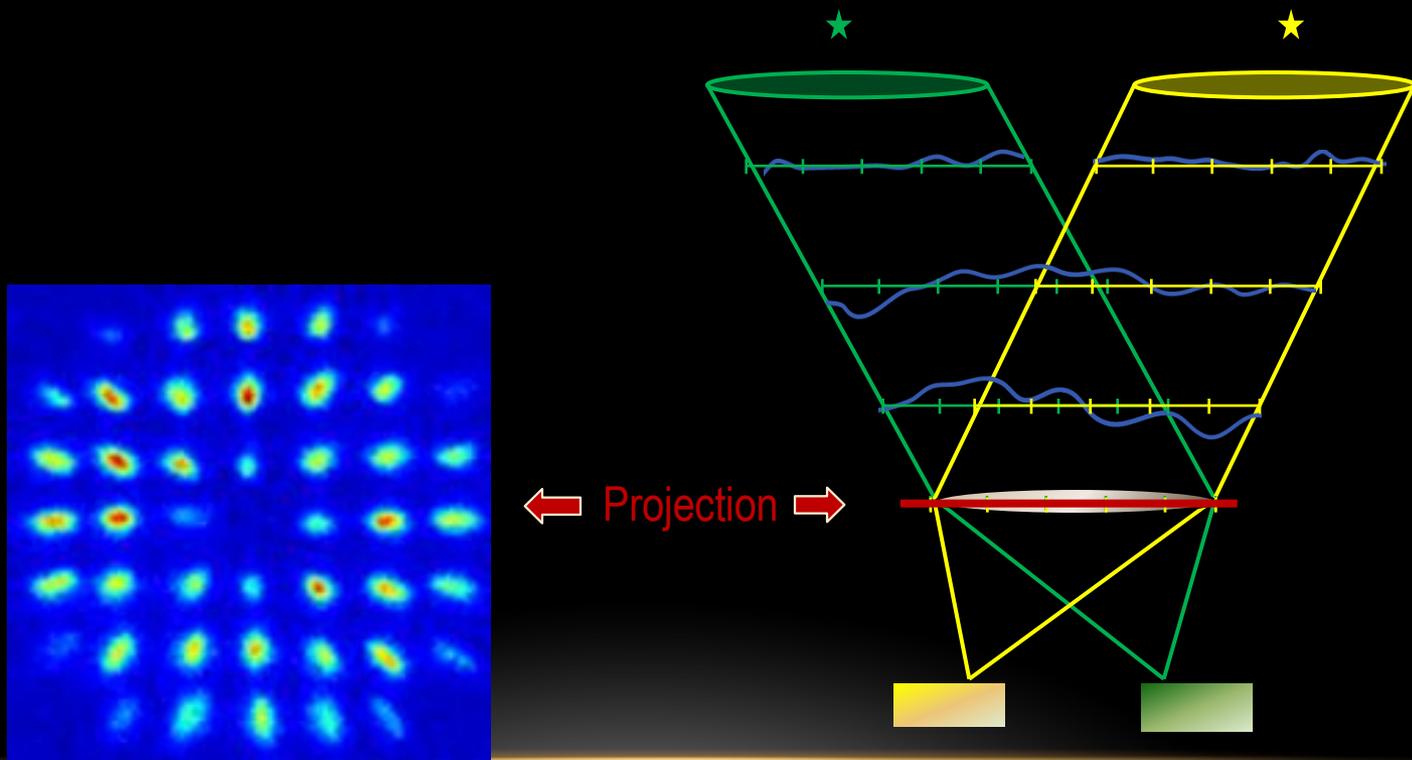
- The majority of future astronomical Adaptive Optics systems will use some form of **wavefront tomography**
 - Tomographic wavefront sensing allows us to:
 - Perform **wide field of view** correction
 - Use **multiple laser guide star systems** efficiently
 - Controlling a tomographic AO system optimally places some additional requirements on the deformable mirror
 - In this talk I aim to provide:
 - A (very brief) overview of how we perform tomography
 - A discussion of the main issues relating to performing tomography
 - Some results from the CANARY on-sky AO demonstrator
 - A description of my 'perfect' DM
-

WAVEFRONT TOMOGRAPHY

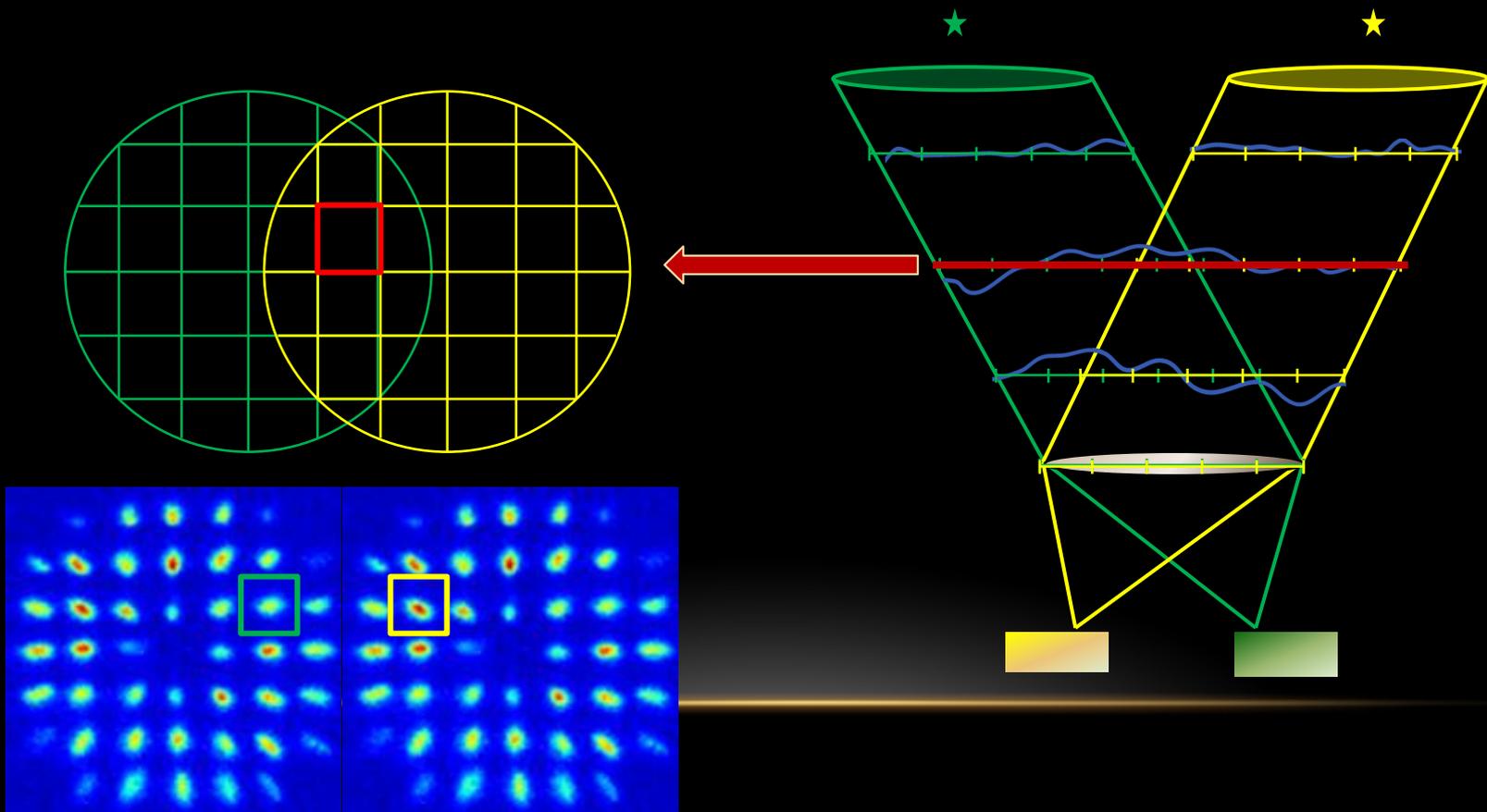


WAVEFRONT TOMOGRAPHY

- Projection of wavefront sensors as they move up in altitude:

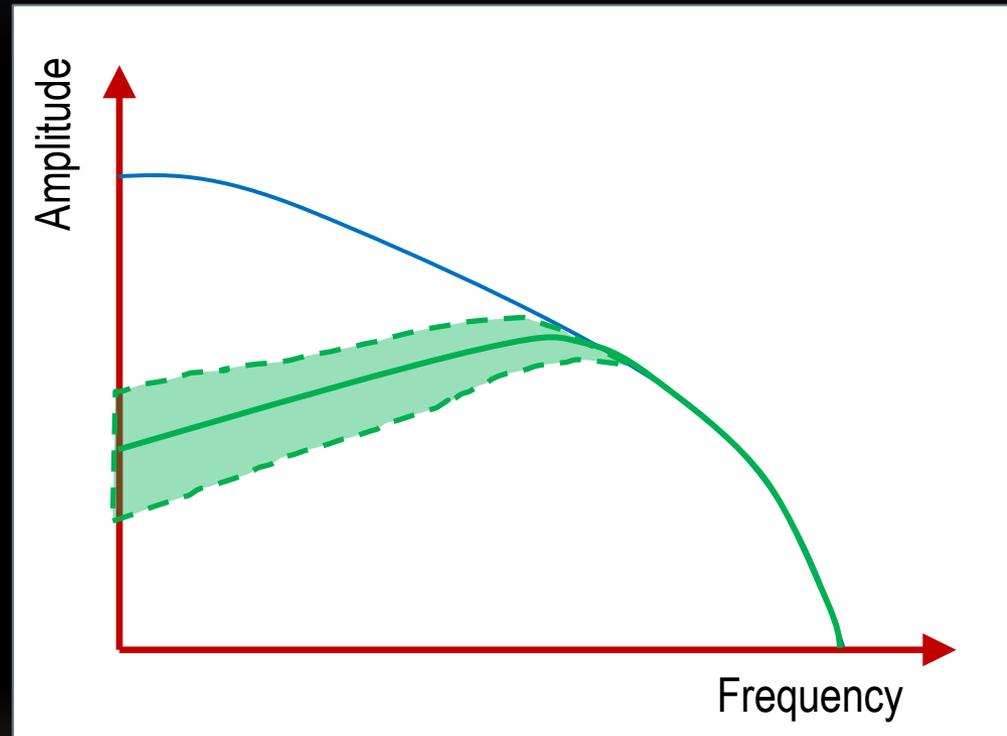


- By comparing common wavefronts between sheared wavefront sensor images



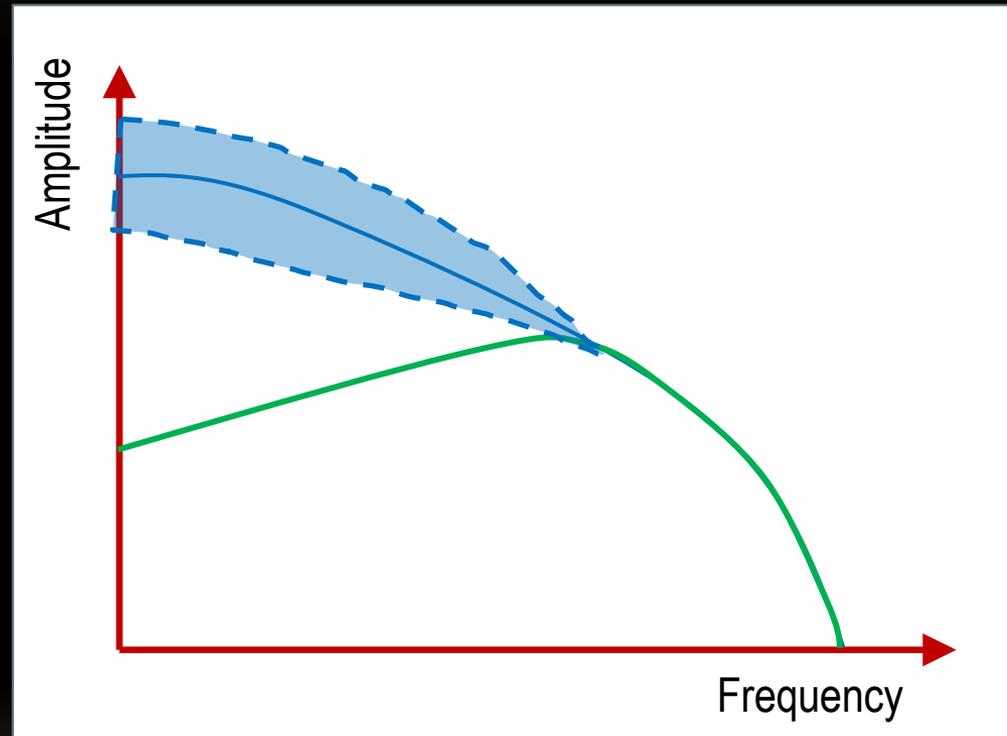
WAVEFRONT TOMOGRAPHY

- Separating the contribution of the different turbulent layers relies on accurate knowledge of the statistical properties of the turbulence under correction
- Atmospheric turbulence obeys a well understood spatial power spectral distribution
- If you run the system in open-loop e.g. MOAO:
 - You end up with an unknown mirror shape that can't be determined directly
 - 'Go-to' error



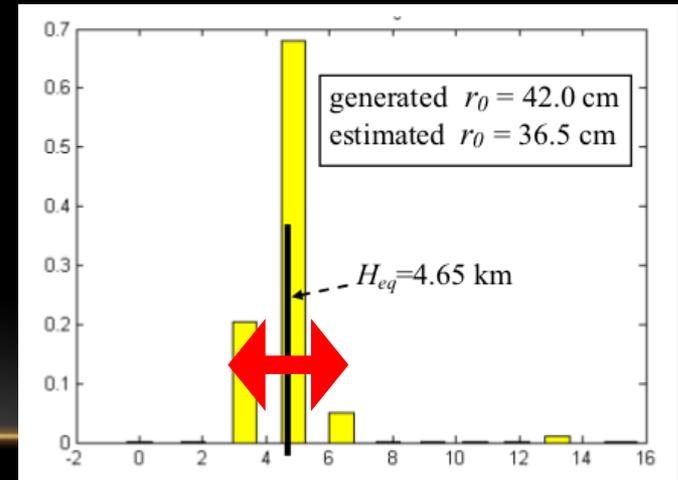
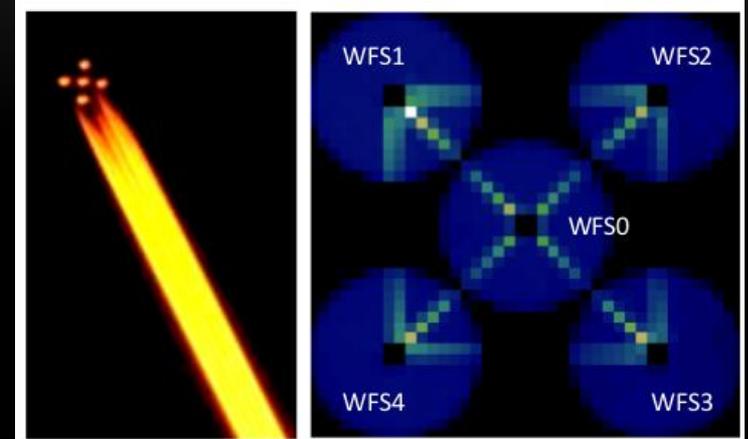
WAVEFRONT TOMOGRAPHY

- If you operate the DM in a closed-loop **tomographic** system e.g. LTAO, MCAO:
 - Optimal performance requires you to reconstruct the uncorrected wavefront slopes
 - Pseudo open-loop slopes
 - Open-loop 'go-to' error becomes an unknown
- Causes errors in measurements of
 - Absolute turbulence strength
 - Thickness of layers
- Impact on PSF reconstruction?



EXAMPLE: TURBULENCE PROFILING USING AN MCAO SYSTEM

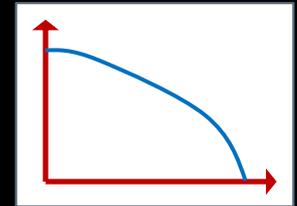
- Cortez *et al*^[1] analysed wavefront sensor data from Gemini South's MCAO system (5 laser guide stars)
- 3 deformable mirrors in the system must be removed to create pseudo-open loop data
- Tested on-sky and using DM-induced turbulence
- Cannot distinguish between WFS errors and open-loop DM errors
- Up to 10% error (worst case) in total turbulence strength estimate
- Influence of a single DM @ 4.5km was spread over 3-7km when WFS data analysed.
- Early results, so it may get better than this
- Scope for further analysis...



[1] Cortez *et al*, <http://arxiv.org/abs/1210.1999> (2012)

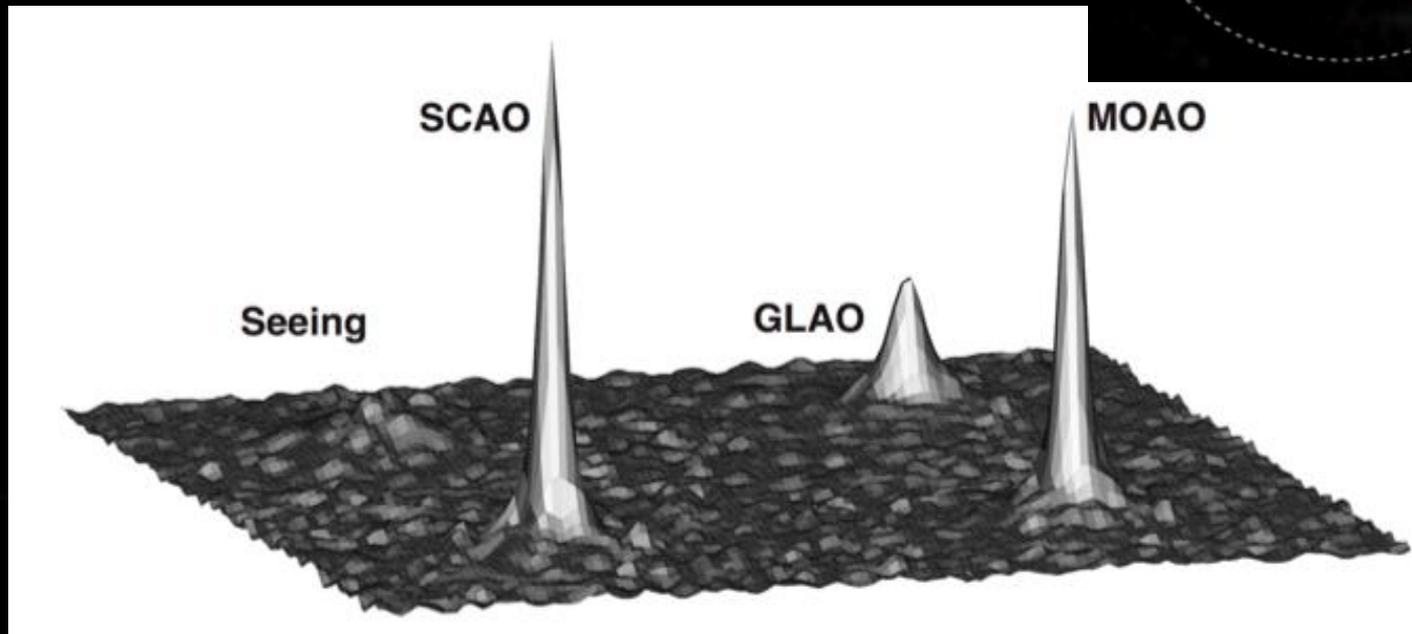
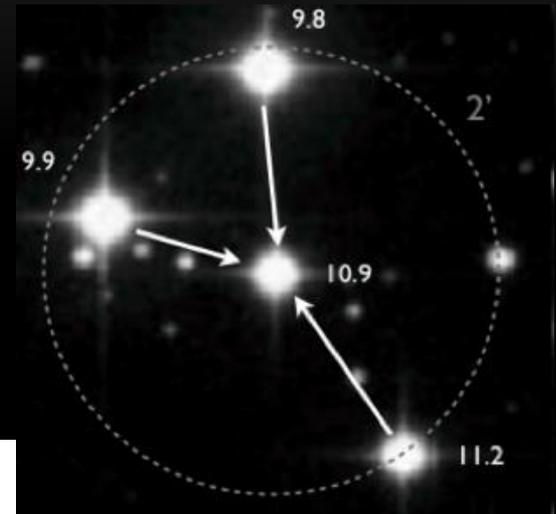
FULLY OPEN-LOOP WITH CANARY

- CANARY is a low-order on-sky tomographic adaptive optics demonstrator that runs in open-loop
 - Phase A: 3 off-axis WFSs measuring uncorrected wavefronts
 - Measured statistics are not 'contaminated'
- AO Correction applied in open-loop on-axis
- A closed loop WFS ('Truth' Sensor)
 - Can measure open-loop error
 - Noise terms have to be removed making analysis complicated
- Initial phase contained a closed-loop DM figure sensor on an internal reference source
 - Precisely to measure the 'go-to' or open-loop error
 - Was also used to control DM shape (briefly)



STREHL RATIO COMPARISON IMAGE

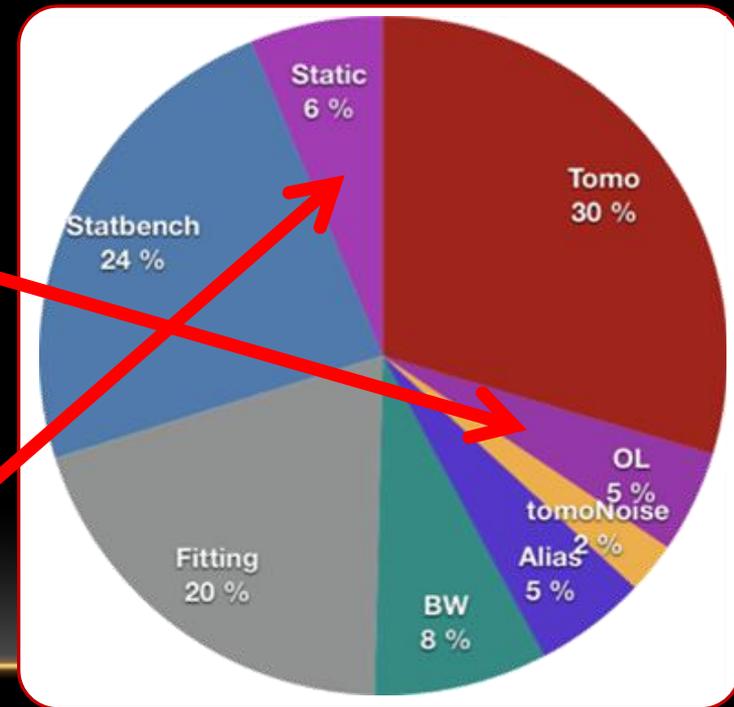
- Images recorded at a central wavelength of $1.495\mu\text{m}$
- Seeing-limited (NoAO) (SR=1% at 00h59mn)
- GLAO (SR=9% at 00h42mn)
- MOAO (SR=19.4% at 00h29mn)
- SCAO (SR=23.8% at 00h32mn)



BACK TO THE ERROR BUDGET...

- Analysed from 7 seconds of synchronised data at 00h10mn12s on Sept 27th Asterism #47)
- 150Hz frame rate, $r_0 = 16.3\text{cm}$ (natural seeing 0.69")

Error	Estimated value (nm rms)
σ^2_{tomo}	168
σ^2_{OL}	68
$\sigma^2_{\text{tomonoise}}$	48
$\sigma^2_{\text{aliasing}}$	71
σ^2_{BW}	88
$\sigma^2_{\text{fitting}}$	137
$\sigma^2_{\text{statbench}}$	150
σ^2_{static}	77
Total	308



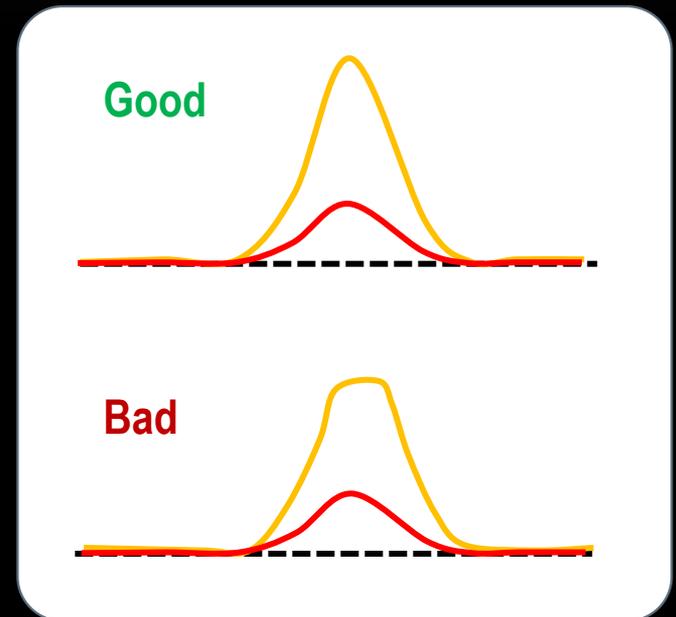
Expected SR = 19.0% @ 1.49 μm => measured = 21%

THE 'PERFECT' TOMOGRAPHIC DM

- EAGLE Phase A study required a **49nm** RMS open-loop error total
 - CANARY has between 68-102nm RMS depending in source of quasi-static term
 - The **open-loop error** has to be small
 - <35nm RMS would make it a minor term in the CANARY error budget
 - Impact on pseudo-open loop reconstruction requires a lot of additional analysis
 - It has to be **stable**
 - The 'quasi-static' shape should remain <35nm RMS over observing period
 - ELT/VLT this would get offloaded to the active optics potentially
 - Maintained over all environmental/gravitational conditions
 - **WE DON'T WANT TO INCORPORATE A FIGURE SENSOR**
 - Not so much of a problem for CANARY, but ELT-scales?
 - Low-order for slowly varying terms is a good option
-

THE 'PERFECT' TOMOGRAPHIC DM

- **Linearity** not so much of an issue, but influence functions must be reproducible
 - Actuator response to voltage/charge need not be linear
 - Relatively minor computational overhead
- **Linear summation** of actuators should be valid
 - Additional computation if it's not
 - Cross-coupling not an issue
- Influence functions must **retain shape** from small to large influence
- **Actuator yield** is not critical for most AO applications
 - Strehl loss (*very rough worst case*) is $N_{\text{failed}}/N_{\text{total}}$
 - 1-3 actuators per 100?



CONCLUSION

- Irrespective of whether you run in open- or closed-loop, tomographic AO system performance is improved by an open-loop capable DM
 - Places additional requirements on DM stability
 - Many of the requirements are already being addressed
 - Calibration is key!
-